

# Analysis of Water Oxidation Catalysis by Dinuclear Ruthenium Complex $[(\text{NH}_3)_5\text{Ru}-\text{O}-\text{Ru}(\text{NH}_3)_5]^{4+}$ Incorporated in a Nafion<sup>®</sup> Membrane

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Catalytic activity of a dinuclear ammine ruthenium complex,  $[(\text{NH}_3)_5\text{Ru}-\text{O}-\text{Ru}(\text{NH}_3)_5]^{4+}$ , for water oxidation to evolve  $\text{O}_2$  was investigated both in homogeneous aqueous solution and in heterogeneous Nafion<sup>®</sup> membrane systems using  $\text{Ce}^{\text{IV}}$  oxidant. It was suggested that the complex works as a four-electron water oxidation catalyst and that the water oxidation by the complex is in competition with a bimolecular decomposition between the complexes. The first-order rate constant ( $k_{\text{O}_2}$  ( $\text{s}^{-1}$ )) for  $\text{O}_2$  evolution and second-order rate constant ( $k_{\text{deact}}$  ( $\text{M}^{-1} \text{s}^{-1}$ )) for bimolecular decomposition were obtained by a kinetic analysis. It was found that  $k_{\text{deact}}$  decreased by one order of magnitude by incorporating the complex in the membrane; this was ascribed to the suppression of the bimolecular decomposition. The critical decomposition distance ( $r_d$  (nm)) between the catalysts was analyzed to be 1.06 nm based on an intermolecular distance distribution.

Heterogeneous polymer membrane systems incorporating functional molecules such as a sensitizer,<sup>1</sup> redox center,<sup>2,3</sup> probe,<sup>4</sup> and catalyst<sup>5–8</sup> have been extensively studied for designing molecule-based photoelectric devices.<sup>9</sup> It is important to elucidate the factors affecting functions of the molecule and to derive an activity model involving these factors in order to optimize the functions of the molecule-based devices.

Water oxidation catalyst is one of the interesting candidates as a functional molecule because water oxidation is not only a fundamental catalysis process in nature, but is also important in photochemical solar energy conversion systems.<sup>10</sup> Many heterogeneous water oxidation catalyst systems have been reported.<sup>11–13</sup> However, there has been no report on an activity model, in which the factors affecting the catalyst activity are evaluated and involved in the theoretical equation, except our reports.<sup>8,14,15</sup>

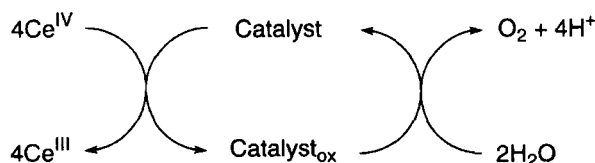
We have reported heterogeneous water oxidation catalyses by mononuclear ruthenium complexes,  $[\text{Ru}(\text{NH}_3)_5\text{Cl}]^{2+14a}$  and  $[\text{Ru}(\text{NH}_3)_6]^{3+14b}$ , and a trinuclear ruthenium complex, Ru-red ( $[(\text{NH}_3)_5\text{Ru}-\text{O}-\text{Ru}(\text{NH}_3)_4-\text{O}-\text{Ru}(\text{NH}_3)_5]^{6+}$ )<sup>15</sup> using  $\text{Ce}^{\text{IV}}$  oxidant as shown in Scheme 1. It is of great interest to analyze the catalyst activity of a dinuclear ruthenium com-

plex for water oxidation and to compare it with the mono- and trinuclear ruthenium complexes reported earlier<sup>14,15</sup> for designing an active and stable molecule-based catalyst. In the present work,  $[(\text{NH}_3)_5\text{Ru}-\text{O}-\text{Ru}(\text{NH}_3)_5]^{4+}$  ( $\text{RuORu}^{4+}$ ) was found to be an active 4-electron water oxidation catalyst. The activity of the  $\text{RuORu}^{4+}$  catalyst in a Nafion<sup>®</sup> membrane will be analyzed based on intermolecular distance distribution, and the effect of the multinuclear structure on multi-electron behavior will be presented.

## Experimental

**Materials and Preparation.**  $[(\text{NH}_3)_5\text{Ru}-\text{O}-\text{Ru}(\text{NH}_3)_5](\text{PF}_6)_4$  complex was prepared according to the procedure of Meyer et al.<sup>16</sup> by oxidation of  $[\text{Ru}(\text{NH}_3)_5\text{H}_2\text{O}](\text{PF}_6)_2$  using  $\text{LiClO}_4$  as oxidant in acetone containing  $[\text{N}(n\text{-C}_4\text{H}_9)_4](\text{PF}_6)$ . Cerium(IV) diammonium nitrate was purchased from Wako Pure Chemical Industries, and  $[\text{Ru}(\text{NH}_3)_5\text{Cl}]\text{Cl}_2$  and Nafion<sup>®</sup> 117 membrane (thickness 180  $\mu\text{m}$ ) from Aldrich Chemical Co. Inc..

**Preparation of Nafion Membrane Incorporating  $\text{RuORu}^{4+}$ .** Nafion<sup>®</sup> membrane was sufficiently swollen by soaking in distilled water for ca. 24 h. The swollen membranes were immersed in aqueous complex solutions (3 ml) with different concentrations for ca. 5 h to incorporate the complex into the membrane by cation exchange. The theoretical cation-exchange capacity of the Nafion<sup>®</sup> membrane is estimated to be  $3.5 \times 10^{-1} \text{ mol dm}^{-3}$  for the  $\text{RuORu}^{4+}$  with four valence since the concentration of sulfonate group in a Nafion<sup>®</sup> membrane is reported to be  $1.4 \text{ mol dm}^{-3}$ .<sup>15</sup> The degree of cation-exchange by the  $\text{RuORu}^{4+}$  was calculated to be 0.26–33% under the present concentration conditions. The complex amount in the membrane was estimated from the absorbance change of the aqueous solution before and after adsorption of the complex. The complex concentration in the membrane was calculated from the complex amount and the membrane volume before swelling. The complex incorporated in the membrane was not dissolved into water during catalysis using  $\text{Ce}(\text{IV})$  oxidant.



Scheme 1. Chemical water oxidation catalysis.

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**Measurements.** In a homogeneous aqueous solution system, excess Ce(NH<sub>4</sub>)<sub>2</sub>(NO<sub>3</sub>)<sub>6</sub> oxidant ( $6.0 \times 10^{-3}$  mol) was added quickly to  $5.0 \times 10^{-5}$ – $9.0 \times 10^{-3}$  M complex aqueous solution (5.0 ml) in a reaction vessel ( $1 \text{ M} = 1 \text{ mol dm}^{-3}$ ). In the heterogeneous Nafion<sup>®</sup> membrane system, the membrane ( $1.1 \times 10^{-4} \text{ dm}^3$ ) that incorporated  $1.0 \times 10^{-7}$ – $1.25 \times 10^{-5}$  mol complex was put into pure water in a reaction vessel, and excess Ce<sup>IV</sup> oxidant ( $4.0 \times 10^{-3}$  mol) was added quickly. In both the systems, the atmosphere in the reaction vessel was replaced with argon gas before adding the Ce<sup>IV</sup> oxidant. For all the experiments, the vessel was kept at 25 °C. The pH was 0.43 without any buffer under the whole complex concentration range under the typical conditions, and the pH change was less than 0.03 before and after the O<sub>2</sub> evolution experiment. The O<sub>2</sub> evolved was analyzed on a gas chromatograph equipped with a molecular sieve 5A column using argon carrier gas (flow rate is  $40 \text{ ml min}^{-1}$ ) at 50 °C. The sensitivity and accuracy of gas chromatography are 100 ppm and  $\pm 1\%$ , respectively, and ca.  $1 \mu\text{l}$  of O<sub>2</sub> evolved is exactly detected under the present conditions. O<sub>2</sub> from atmospheric contamination can be negligible because O<sub>2</sub> and N<sub>2</sub> were not at all detected in control experiments without the catalyst. In the present system, bubbles of O<sub>2</sub> can be observed.

### Results and Discussion

A typical time dependence of the amount of O<sub>2</sub> evolved in the Nafion<sup>®</sup> membrane system is shown in Fig. 1. The O<sub>2</sub> evolved increased linearly with time at the initial stage (up to ca. 45 min) as shown in the inset of Fig. 1, and then gradually declined but did not saturate even after 8 h. The initial O<sub>2</sub> evolution rate ( $V_{\text{O}_2}$  (mol s<sup>-1</sup>)) was obtained from the initial slope.

When assuming that 4-electron water oxidation to evolve O<sub>2</sub> is catalyzed by one molecule of the complex which has 4-electron oxidation ability, the overall O<sub>2</sub> evolution consists of oxidation of the (catalyst)<sub>red</sub> (the reduced form of catalyst) by the 1-electron Ce<sup>IV</sup> oxidant (Eq. 1) and 4-electron water oxidation by one (catalyst)<sub>ox</sub> (their oxidized form) (Eq. 2).

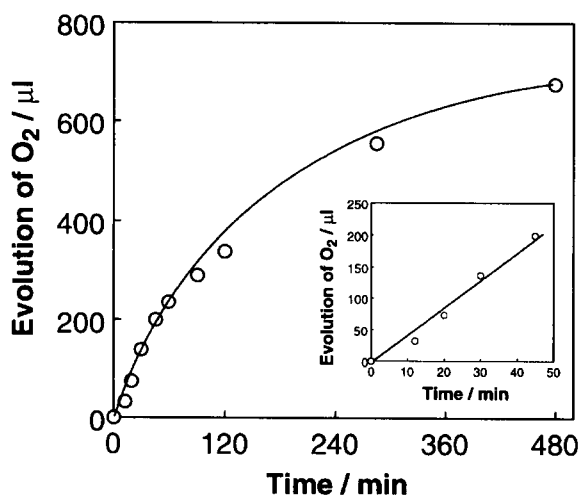
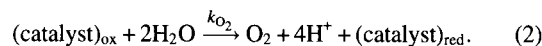
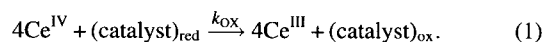


Fig. 1. Time dependence of the amount of O<sub>2</sub> evolved in water oxidation in the Nafion<sup>®</sup> membrane system using Ce<sup>IV</sup> oxidant. The inset shows the data in the initial stage. The amounts of catalyst and oxidant are  $5.0 \times 10^{-7}$  mol and  $4.0 \times 10^{-3}$  mol, respectively, in  $10.0 \text{ cm}^3$  water. Membrane volume,  $1.1 \times 10^{-4} \text{ dm}^3$ .



The O<sub>2</sub> evolution rate is given by the Eq. 3 using a steady-state method when assuming that the reaction rate in Eq. 1 is expressed by  $k_{\text{ox}} [\text{Ce}^{\text{IV}}]^4 [\text{catalyst}]$ :<sup>15</sup>

$$\begin{aligned} \frac{d[\text{O}_2]}{dt} &= (V_{\text{O}_2}/v) = \frac{k_{\text{O}_2} k_{\text{ox}} [\text{Ce}^{\text{IV}}]^4 [\text{catalyst}]}{k_{\text{ox}} [\text{Ce}^{\text{IV}}]^4 + k_{\text{O}_2}} \\ &= \frac{k_{\text{O}_2} [\text{catalyst}]}{1 + k_{\text{O}_2}/(k_{\text{ox}} [\text{Ce}^{\text{IV}}]^4)}, \end{aligned} \quad (3)$$

where  $v$  (dm<sup>3</sup>) is the aqueous solution volume or membrane volume,  $k_{\text{ox}}$  (M<sup>-4</sup> s<sup>-1</sup>) and  $k_{\text{O}_2}$  (s<sup>-1</sup>) are the rate constant for the reaction in Eq. 1 and the pseudo first order rate constant for the reaction in Eq. 2, respectively.

The  $V_{\text{O}_2}$  increased with the increase in the Ce<sup>IV</sup> concentration, and then was saturated beyond ca. 100 molar ratio of Ce<sup>IV</sup>/complex. The almost constant  $V_{\text{O}_2}$  value saturated beyond this molar ratio of Ce<sup>IV</sup>/complex shows that the term  $k_{\text{O}_2}/(k_{\text{ox}} [\text{Ce}^{\text{IV}}]^4)$  is negligible in the Eq. 3, i.e., the value of  $k_{\text{ox}} [\text{Ce}^{\text{IV}}]^4$  is large enough in comparison with the  $k_{\text{O}_2}$  value, so that the reaction in Eq. 2 is a rate determining-step for O<sub>2</sub> evolution under the large excess Ce<sup>IV</sup> conditions. Therefore,  $V_{\text{O}_2}$  at a large excess of Ce<sup>IV</sup> oxidant (beyond ca. 100 of the molar ratio of Ce<sup>IV</sup>/complex) is given as

$$\frac{d[\text{O}_2]}{dt} = (V_{\text{O}_2}/v) = k_{\text{O}_2} [\text{catalyst}], \quad (4)$$

showing that the  $V_{\text{O}_2}$  is first order with respect to the complex concentration according to Eq. 4 under the large excess Ce<sup>IV</sup> conditions. All the O<sub>2</sub> evolution experiments were carried out under the conditions of a large excess Ce<sup>IV</sup> oxidant (the molar ratio of Ce<sup>IV</sup>/complex was at least 130).

The plots of  $V_{\text{O}_2}$  vs. complex concentration in the aqueous solution and membrane systems are shown in Fig. 2 (a) and (b), respectively. These plots increased with the concentration, then exhibited an optimum  $V_{\text{O}_2}$ , and thereafter decreased with the concentration. These plots gave a linearity at low concentrations for both the systems, as shown in the insets of Fig. 2 (a) and (b), showing that water oxidation is first order with respect to the complex concentration. The  $k_{\text{O}_2}$  values in the present aqueous solution and membrane systems were estimated as  $1.5 \times 10^{-2} \text{ s}^{-1}$  and  $1.3 \times 10^{-2} \text{ s}^{-1}$ , respectively, from the slope in the insets of Fig. 2 (a) and (b) according to Eq. 4, showing that the intrinsic catalytic activity in the membrane is almost the same as the aqueous solution system.

We have studied the water oxidation catalyses by various mono- and multinuclear complexes. In the [(NH<sub>3</sub>)<sub>5</sub>Ru–O–Ru(NH<sub>3</sub>)<sub>4</sub>–O–Ru(NH<sub>3</sub>)<sub>5</sub>]<sup>6+</sup> system,<sup>15</sup> the plots of  $V_{\text{O}_2}$  vs. complex concentration at low concentrations gave a linear relationship under the conditions of much excess Ce<sup>IV</sup> oxidant, while in the mononuclear complex systems such as [Ru(NH<sub>3</sub>)<sub>5</sub>Cl]<sup>2+</sup><sup>14a</sup> and [Ru(NH<sub>3</sub>)<sub>6</sub>]<sup>3+</sup><sup>14b</sup>, these plots gave clearly second-order dependency with respect to the complex concentration. This indicates that even in the presence of much excess of Ce<sup>IV</sup>, the mechanism is reflected in the dependency of  $V_{\text{O}_2}$  on the catalyst concentration. It is

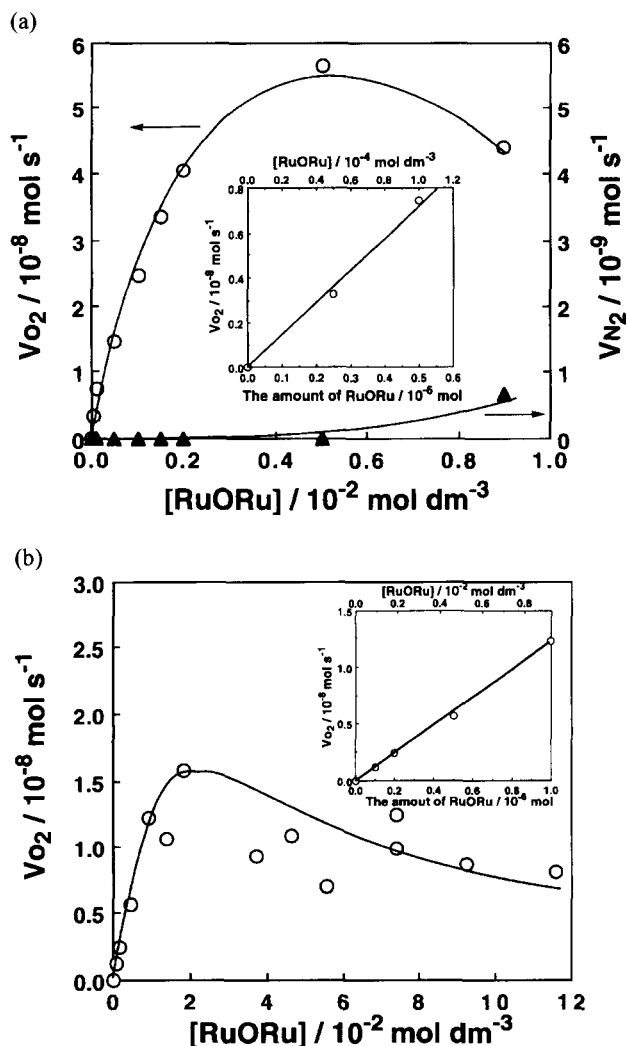


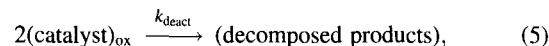
Fig. 2. (a) Dependencies of initial  $O_2$  evolution rate,  $V_{O_2}$  ( $\text{mol s}^{-1}$ ), (O) and  $N_2$  evolution rate,  $V_{N_2}$  ( $\text{mol s}^{-1}$ ), ( $\blacktriangle$ ) on complex concentration in aqueous solution system. The inset shows data in low concentration regions. liquid volume,  $5.0 \text{ cm}^3$ ;  $\text{Ce}^{\text{IV}}$ ,  $6.0 \times 10^{-3} \text{ mol}$ . (b) Dependence of initial  $O_2$  evolution rate,  $V_{O_2}$  ( $\text{mol s}^{-1}$ ), (O) on complex concentration in Nafion<sup>®</sup> membrane system. The inset shows data in low concentration regions. Membrane volume,  $1.1 \times 10^{-4} \text{ dm}^3$ ;  $\text{Ce}^{\text{IV}}$ ,  $4.0 \times 10^{-3} \text{ mol}$  in  $10.0 \text{ cm}^3$  water.

reasonable, based on the redox reactions of these complexes, that the difference in the concentration dependencies of  $V_{O_2}$  is explained by the difference in the ability of catalytic water oxidation (4- or 2-electron oxidation). Most probably, the linear plots of  $V_{O_2}$  vs. complex concentration in the insets of Fig. 2 (a) and (b) would show that the present dinuclear complex works as a 4-electron oxidation catalyst. Multinuclear structure must be an important factor to construct a four-electron water oxidation catalyst.

The active species might be  $\text{Ru}^{\text{V}}\text{--Ru}^{\text{V}}$  in the 4-electron water oxidation by one molecule. The redox reaction of  $\text{RuORu}^{4+}$  was reported by Meyer to indicate the reversible redox of  $\text{RuORu}^{4+}/\text{RuORu}^{5+}$  at 0.32 V (vs. saturated sodium chloride calomel electrode) and irreversible further oxidation

to  $\text{RuORu}^{6+}$  at 1.67 V in the cyclic voltammogram (CV) of  $\text{RuORu}^{4+}$  in an acetonitrile solution, though the second oxidation is not well-defined.<sup>16</sup> In our earlier report on the CV of a Nafion<sup>®</sup> membrane-coated Pt electrode incorporating  $\text{RuORu}^{5+}$  in the potential range of 0.2 V to 1.4 V vs. Ag/AgCl, no redox response other than an unclear irreversible oxidative wave at 1.1 V could be observed before the increased catalytic current on water oxidation.<sup>17</sup> We have reported the CV of a Nafion<sup>®</sup> membrane-coated ITO electrode incorporating  $[\text{Ru}(\text{NH}_3)_5\text{Cl}]^{2+}$  in which two oxidative peaks at 1.06 and 1.28 V vs. SCE (1.30 and 1.52 V vs. NHE) were observed based on  $\text{Ru}^{\text{III}}/\text{Ru}^{\text{IV}}$  and  $\text{Ru}^{\text{IV}}/\text{Ru}^{\text{V}}$ , respectively.<sup>18</sup> Since the real redox potential (in the order of 1.6 V) of the  $\text{Ce}^{\text{IV}}/\text{Ce}^{\text{III}}$  under the present conditions is higher than that (1.52 V vs. NHE) of  $\text{Ru}^{\text{IV}}/\text{Ru}^{\text{V}}$ , it is possible that the  $\text{Ru}^{\text{V}}$  state of  $[\text{Ru}(\text{NH}_3)_5\text{Cl}]^{2+}$  is formed by a  $\text{Ce}^{\text{IV}}$  oxidant. The potential for forming the  $\text{Ru}^{\text{V}}\text{--Ru}^{\text{V}}$  state of the present  $\text{RuORu}^{4+}$  is considered, at least, to be lower than that of  $\text{Ru}^{\text{IV}}/\text{Ru}^{\text{V}}$  in  $[\text{Ru}(\text{NH}_3)_5\text{Cl}]^{2+}$  because of the delocalization of charges, and therefore, the  $\text{Ru}^{\text{V}}\text{--Ru}^{\text{V}}$  state is possible to be formed in the present system.

$N_2$  was evolved at high concentrations only in the aqueous solution system (Fig. 2(a)). Since no  $N_2$  was detected in an aqueous solution containing the same amount of  $\text{Ce}^{\text{IV}}$  without the complex, this  $N_2$  evolved can result only from the oxidation of the ammine ligands of the catalyst.  $V_{N_2}$  is second order with respect to the complex concentration (Fig. 2(a)), showing that bimolecular decomposition of the complexes takes place as described in Eq. 5,



where  $k_{\text{deact}}$  ( $\text{M}^{-1} \text{ s}^{-1}$ ) represents the second-order rate constant for the bimolecular decomposition. This will be supported by a kinetic analysis described later.

In order to analyze the catalyst activities in the aqueous solution and membrane systems, an apparent first-order rate constant of  $O_2$  evolution ( $k_{\text{app}}$  ( $\text{s}^{-1}$ )) was defined as

$$k_{\text{app}} = V_{O_2} / n_{\text{Ru}}, \quad (6)$$

where  $n_{\text{Ru}}$  (mol) is the amount of the complex. The comparison of  $k_{\text{app}}$  between the aqueous solution and membrane systems is possible based on the dependencies of  $k_{\text{app}}$  on the catalyst concentration as shown in Fig. 3. In both the aqueous solution and membrane systems, the  $k_{\text{app}}$  decreased with the increase of the catalyst concentration. However, decreasing tendency of the  $k_{\text{app}}$  is much lower for the membrane system than for the aqueous solution, which can be ascribed to stabilization of the catalyst against bimolecular decomposition due to adsorption of the complex in the membrane.

On the basis of the consideration that the first-order water oxidation by the high oxidation state complex (Eq. 2) is in competition with the bimolecular decomposition of the complex (Eq. 5), Eq. 7 was derived to analyze  $k_{\text{app}}$ :<sup>15</sup>

$$k_{\text{app}}^{-1} = 1/k_{O_2} + (k_{\text{deact}}/k_{O_2}^2)[\text{RuORu}]. \quad (7)$$

According to Eq. 7, plots of  $k_{\text{app}}^{-1}$  vs.  $[\text{RuORu}]$  are shown

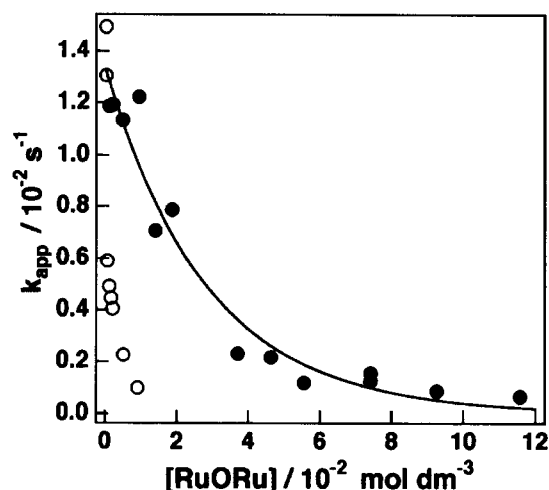


Fig. 3. Relationship between apparent catalytic activity ( $k_{\text{app}}$  ( $\text{s}^{-1}$ )) and complex concentration in the aqueous solution (○) and the membrane systems (●). The solid line is the calculated curve based on Eq. 8.

in Fig. 4 for the aqueous solution and membrane systems. They show linear relationships, supporting the competition between the first-order O<sub>2</sub> evolution and the bimolecular decomposition. The  $k_{\text{O}_2}$  and  $k_{\text{deact}}$  for both the aqueous solution and membrane systems were obtained from the intercept and slope of the straight lines in the Fig. 4, respectively. These

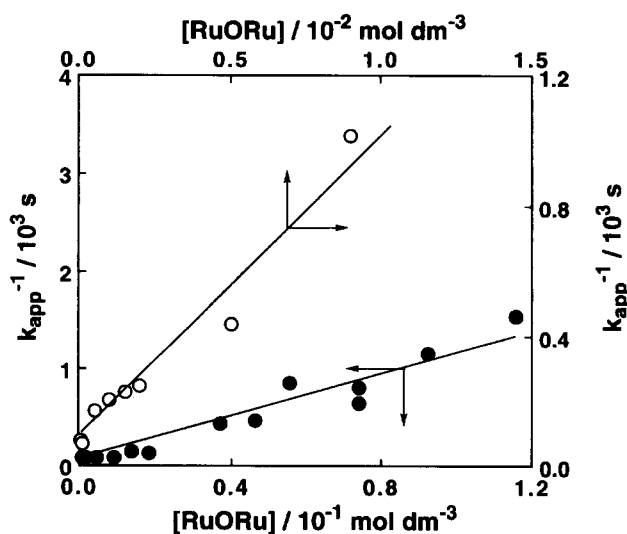


Fig. 4. Plots of  $k_{\text{app}}^{-1}$  versus catalyst concentration in the aqueous solution (○) and the membrane systems (●) according to Eq. 7.

values are listed in Table 1. The  $k_{\text{O}_2}$  values in both the systems are almost the same as those obtained from the initial slope in the insets of Fig. 2 (a) and (b), respectively. The  $k_{\text{deact}}$  value in the membrane system is lower than that in the aqueous solution system by one order of magnitude. In the present system, the cationic complex is electrostatically attached to anionic sulfonate groups on the Nafion<sup>®</sup> chain, so that there is a strong restriction for the complex to move from site-to-site in the membrane, although smaller counter cations can move in the membrane. The bimolecular decomposition was suppressed by the restriction to result in a much lower  $k_{\text{deact}}$  value in the membrane system. This also shows that free diffusion of the catalyst is prohibited in the matrix. Therefore, the bimolecular decomposition could be analyzed by a static mechanism rather than a dynamic one which involves diffusion and collision of the complex in the membrane.

We have reported that the catalytic activity of a molecule-based catalyst in a polymer membrane can be analyzed by using intermolecular distance distribution.<sup>14,15</sup> When assuming that the catalysts existing within a critical decomposition distance,  $r_d$  (nm), undergo a bimolecular decomposition,  $k_{\text{app}}$  is represented by Eq. 8:

$$k_{\text{app}} = k \times \exp \left\{ -4\pi(r_d^3 - s^3)acN_A \times 10^{-24}/3 \right\}, \quad (8)$$

Table 1. Rate Constants  $k_{\text{O}_2}$  and  $k_{\text{deact}}$  Obtained from Fig. 4 and Eq. 7

System	$k_{\text{O}_2} / 10^{-2} \text{ s}^{-1}$	$k_{\text{deact}} / \text{dm}^3 \text{ mol}^{-1} \text{ s}^{-1}$
Aqueous solution	1.3 (1.5) <sup>a</sup>	20.7
Nafion <sup>®</sup> membrane	1.3 (1.3) <sup>a</sup>	1.9

a) Obtained from inset of Fig. 2 (a) and (b).

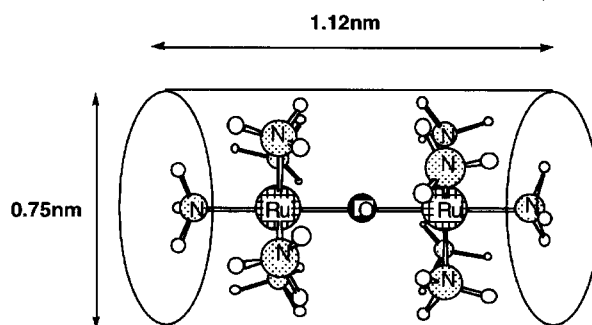


Fig. 5. Steric chemical structure and molecular size of  $\text{RuORu}^{4+}$  complex.

Table 2. Values of Intrinsic Activity  $k$  and Critical Decomposition Distance  $r_d$  for Various Ammine Ruthenium Complexes as Water Oxidation Catalyst Incorporated into a Nafion<sup>®</sup> Membrane

Catalyst	$k / 10^{-2} \text{ s}^{-1}$	$r_d / \text{nm}$	$s / \text{nm}^a$	Mechanism	Reference
$[(\text{NH}_3)_5\text{RuORu}(\text{NH}_3)_4\text{ORu}(\text{NH}_3)_5]^{6+}$ (Ru-red)	4.4	1.23	1.06	4-Electron oxidation	Ref. 14
$[(\text{NH}_3)_5\text{RuORu}(\text{NH}_3)_5]^{4+}$	1.3	1.06	0.98	4-Electron oxidation	Present system
$[\text{Ru}(\text{NH}_3)_5\text{Cl}]^{2+}$	0.27	0.84	0.75	2-Electron oxidation	Ref. 15

a) Molecular diameter approximated as a sphere.

where  $k$  ( $\text{s}^{-1}$ ),  $s$  (nm),  $\alpha$ ,  $c$  ( $\text{mol dm}^{-3}$ ) and  $N_A$  ( $\text{mol}^{-1}$ ) are an intrinsic activity of the catalyst, contact distance (0.98 nm) between the complexes, localization degree (40)<sup>15</sup> of the complex in the Nafion® membrane, complex concentration in the membrane and Avogadro's number, respectively. This  $s$  value was tentatively taken as the radius of a sphere which has the same volume as the complex volume with a cylindrical form (see Fig. 5) in the same way as in our earlier paper.<sup>15</sup> The exponential term of Eq. 8 expresses the fraction of the complex which does not undergo the bimolecular decomposition. Equation 8 was applied to the plots of  $k_{\text{app}}$  vs.  $c$  for the membrane system in Fig. 3 using a nonlinear least-square method, and the best fitting was obtained when  $k$  and  $r_d$  values were  $1.3 \times 10^{-2} \text{ s}^{-1}$  and 1.06 nm, respectively. The  $k$  is the same as the  $k_{\text{O}_2}$  ( $1.3 \times 10^{-2} \text{ s}^{-1}$ ) value calculated from the initial slope in the inset of Fig. 2(b).

The  $k$  and  $r_d$  values<sup>14,15</sup> in various ammine ruthenium complexes/Nafion® membrane are shown in Table 2. The order of the catalytic activity is as follows; Ru-red > RuORu<sup>4+</sup> >> [Ru(NH<sub>3</sub>)<sub>5</sub>Cl]<sup>2+</sup>. The  $k_{\text{O}_2}$  values of di- and trinuclear complexes are remarkably larger than that of the mononuclear complex. These multinuclear complexes are highly active catalysts most probably because they could work as four-electron water oxidation catalyst, while the mononuclear complex needs two molecules for O<sub>2</sub> evolution. Multinuclear structure is important for constructing efficient artificial molecule-based catalysts. Further, the trinuclear complex is more active than RuORu<sup>4+</sup>, suggesting that it is capable of forming a highly oxidized intermediate compared with that of RuORu<sup>4+</sup> due to delocalization of the charges. The order of  $r_d$  is as follows: Ru-red > RuORu<sup>4+</sup> > [Ru(NH<sub>3</sub>)<sub>5</sub>Cl]<sup>2+</sup>. This result is reasonable because this order is the same as that of the molecular size of the complex and the  $r_d$  values are close to the molecular size. This supports that static bimolecular decomposition takes place between the neighboring complexes in the membrane. It is important to separate the distance between the catalysts over 1.06 nm for the RuORu<sup>4+</sup> in the Nafion® membrane.

### Conclusion

Catalytic water oxidation activity based on a dinuclear ruthenium complex, [(NH<sub>3</sub>)<sub>5</sub>Ru–O–Ru(NH<sub>3</sub>)<sub>5</sub>]<sup>4+</sup>, was studied in a homogeneous aqueous solution and heterogeneous Nafion membrane using Ce<sup>IV</sup> oxidant. It was suggested that the complex works as a four-electron water oxidation catalyst and the water oxidation by the complex is in competition with a bimolecular decomposition between the complexes. The second-order rate constant ( $k_{\text{deact}}$  ( $\text{M}^{-1} \text{ s}^{-1}$ )) for bimolecular decomposition decreased by one order of magnitude by incorporating the complex in the membrane, showing that the bimolecular decomposition is remarkably suppressed due to adsorption in the Nafion® membrane. The intrinsic catalytic activity ( $k$  ( $\text{s}^{-1}$ )) and critical decomposition distance

( $r_d$  (nm)) of the complex in the membrane system were analyzed based on intermolecular distance distribution, and compared with those of mono- and trinuclear complexes. It was found that multinuclear structure is an important factor for an active artificial water oxidation catalyst. Control of the intermolecular distance between the complexes is important to optimize the water oxidation catalysis in the membrane.

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